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# Multi-physics simulation of mm-wave systems

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gan-on-Silicon Efficient mm-wave euROpean systEm iNtegration plAtform

# Contributors

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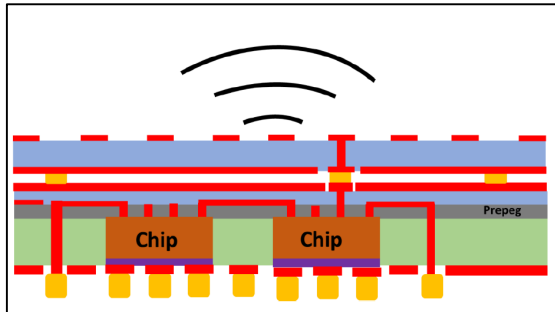
Dr. K. Andersson



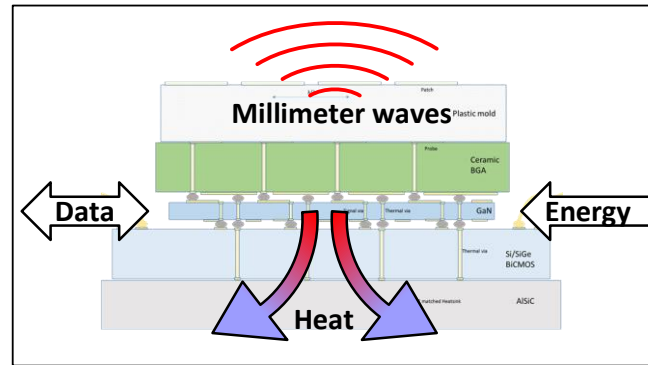
# mm-wave RF systems

- Active antenna arrays
- High integration needed to fit within  $\lambda/2$

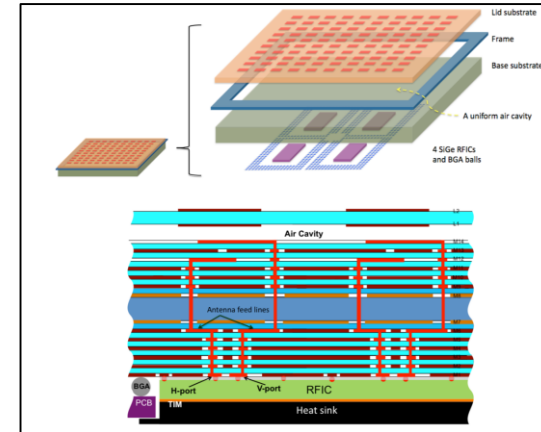
Chip embedding  
(IZM/SERENA)



Vertical stacking

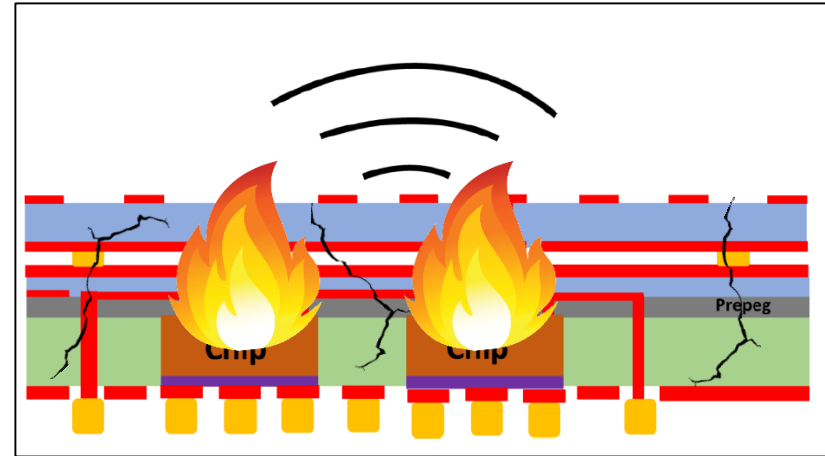


IBM / Ericsson

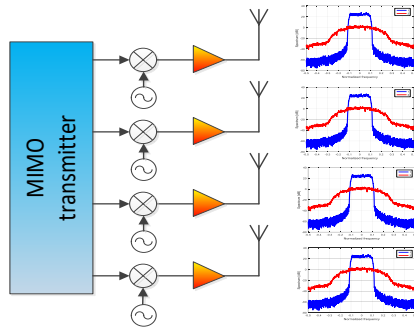


# Challenges

- Multi-physical effects
  - ◆ Electrical
  - ◆ Thermal
  - ◆ Mechanical
  - ◆ ...
- *Efficient simulations and modeling are crucial*
  - ◆ Before: Optimization, reliability, margins, time to market
  - ◆ After: Troubleshooting, performance optimization, reverse engineering



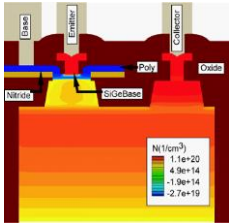
# ELECTRICAL SIMULATIONS



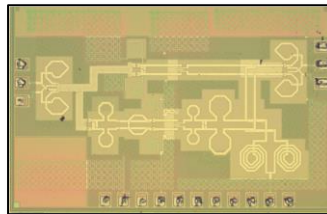
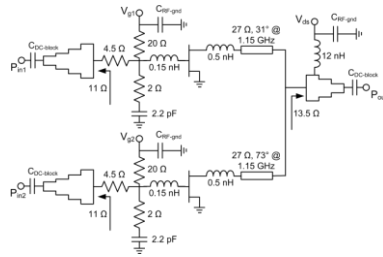
Active antenna arrays  
Antenna-circuit interactions  
Linearity

# Simulations at many levels...

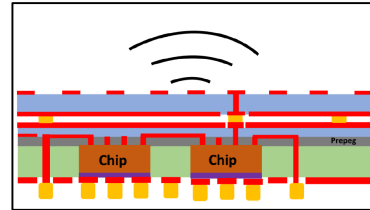
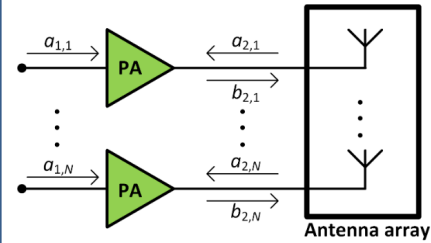
## Transistor



## Circuit

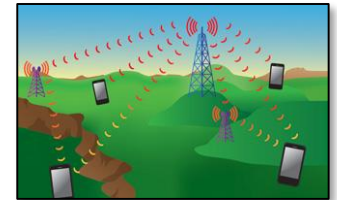


## RF Sub-system



## System

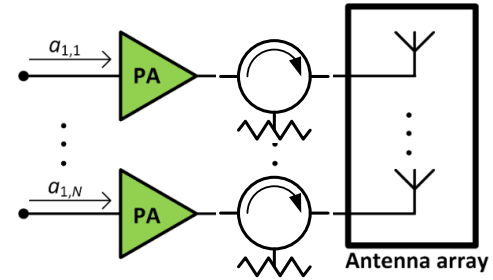
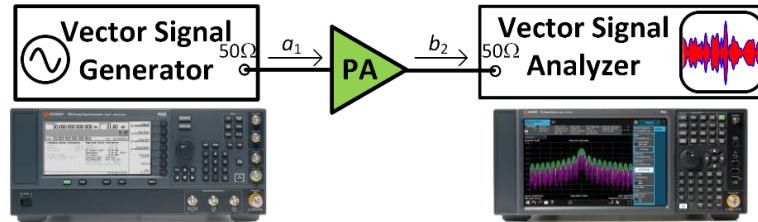
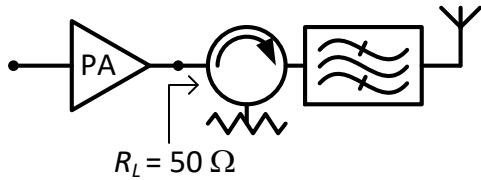
$$y = Hx + w$$



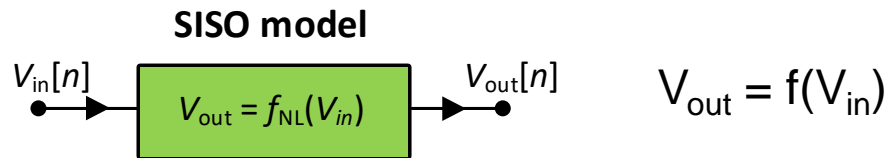
[T. Svensson, Chalmers]

# Transmitter modeling

- Traditionally  $50\Omega$  assumed



- Single-input-single-output modeling of RF components

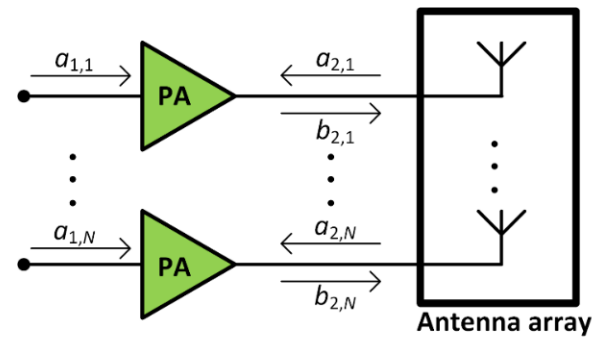
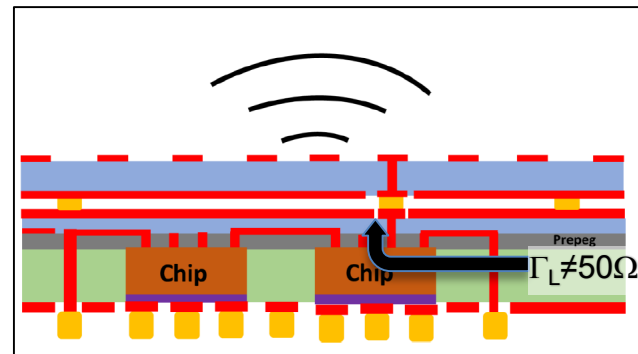


# Transmitter modeling

- Integrated transmitters
  - ◆ Mismatch and mutual coupling
  - ◆ Non-50Ω interfaces

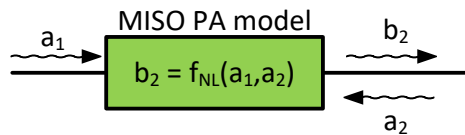
- Dual-input models needed:  

$$b_2 = f(a_1, a_2)$$





# Dual-input behavioral modeling



$$b_2 = \underbrace{\sum_{p_1=1}^{P_1} \alpha_{p_1} |a_1|^{2(p_1-1)} a_1}_{S_{21}(|a_1|)} + \underbrace{\sum_{p_2=1}^{P_2} \beta_{p_2} |a_1|^{2(p_2-1)} a_2}_{S_{22}(|a_1|)} + \underbrace{\sum_{p_2=2}^{P_2} \gamma_{p_2} a_1^2 |a_1|^{2(p_2-2)} a_2^*}_{T_{22}(a_1)}$$

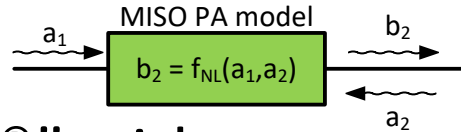
Nonlinear  
50Ω SISO-terms

Nonlinear mismatch terms

- “PHD” or “X-parameter®” model

[Verspecht and D. E. Root, “Polyharmonic distortion modeling,” IEEE Microw. Mag., vol. 7, no. 3, pp. 44-57, Jun. 2006.]

# Dual-input behavioral modeling



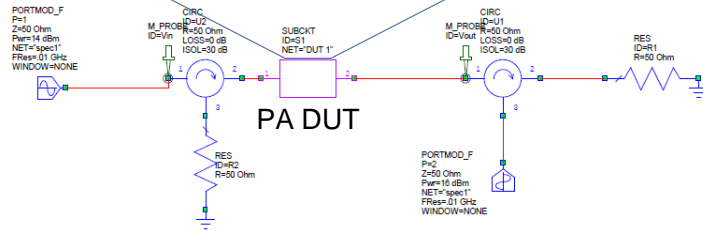
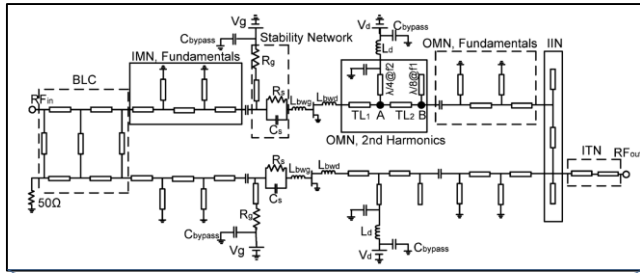
- “X-parameters<sup>®</sup>” with memory

$$\begin{aligned}
 b_2[n] = & \underbrace{\sum_{m_1=0}^{M_1} \sum_{p_1=1}^{P_1} \alpha_{m_1,p_1} |a_1[n-m_1]|^{2(p_1-1)} a_1[n-m_1]}_{S_{21}(|a_1|)} + \\
 & \underbrace{\sum_{m_2=0}^{M_2} \sum_{m_1=0}^{M_1} \sum_{p_2=1}^{P_2} \beta_{m_1,m_2,p_2} |a_1[n-m_1]|^{2(p_2-1)} a_2[n-m_2]}_{S_{22}(|a_1|)} + \\
 & \underbrace{\sum_{m_2=0}^{M_2} \sum_{m_1=0}^{M_1} \sum_{p_2=2}^{P_2} \gamma_{m_1,m_2,p_2} a_1^2[n-m_1] |a_1[n-m_1]|^{2(p_2-2)} a_2^*[n-m_2]}_{T_{22}(a_1)}
 \end{aligned}$$

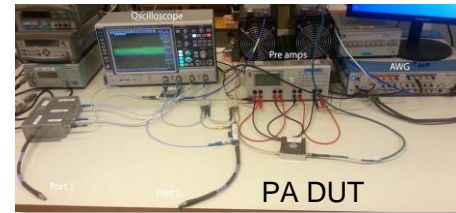
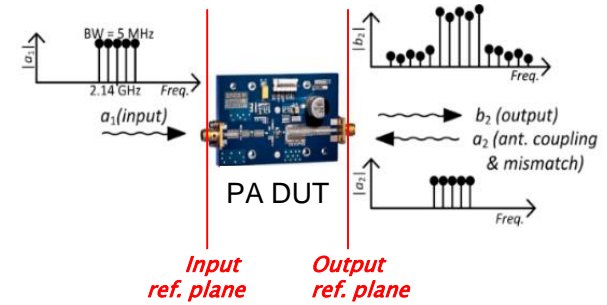
[C. Fager et al., "Prediction of Smart Antenna Transmitter Characteristics Using a New Behavioral Modeling Approach," *Proc. IMS*, 2014]

# Model identification

## Simulation based



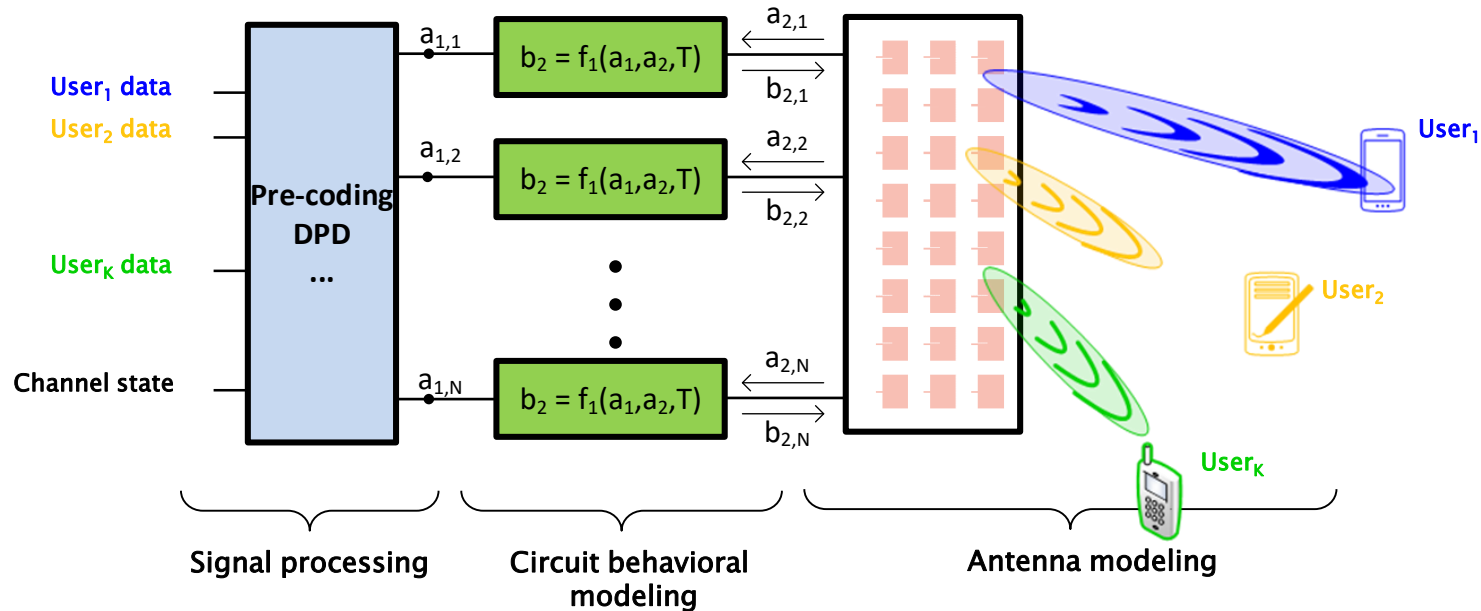
## Measurement based



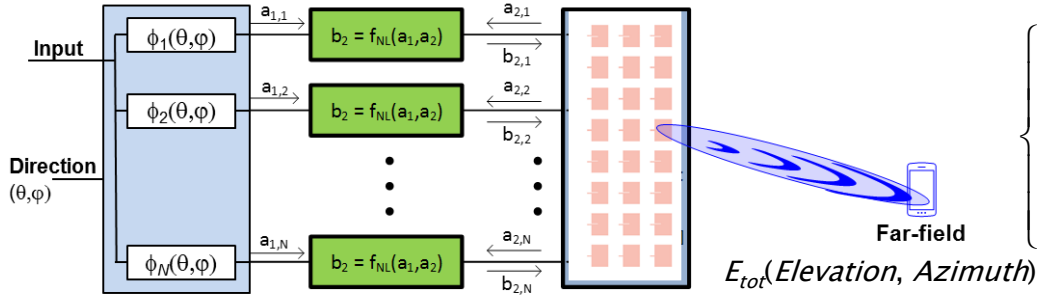
[S. Gustafsson et al., "A Novel Active Load-pull System with Multi-Band Capabilities," ARFTG, 2013]

[C. Fager et al., "Prediction of Smart Antenna Transmitter Characteristics Using a New Behavioral Modeling Approach," Proc. IMS, 2014]

# Transmitter simulation framework



# Phased array application



## Beam steering

$$\begin{cases} \mathbf{a}_1 = a_1 [e^{j\phi_1} & e^{j\phi_2} & \dots & e^{j\phi_N}]^T \\ \mathbf{b}_2 = \mathbf{S}_{21}(|\mathbf{a}_1|)\mathbf{a}_1 + \mathbf{S}_{22}(|\mathbf{a}_1|)\mathbf{a}_2 + \mathbf{T}_{22}(\mathbf{a}_1)\mathbf{a}_2^* \\ \mathbf{a}_2 = \mathbf{S}_{ant}\mathbf{b}_2 \end{cases}$$

## Antenna circuit interactions

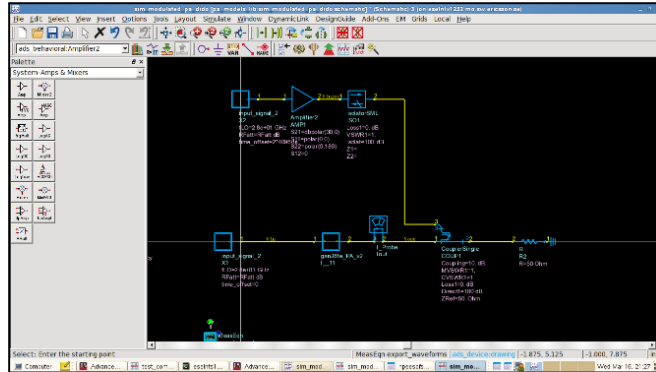
$$\mathbf{b}_2 = \underbrace{\mathbf{S}_{21}(|\mathbf{a}_1|)\mathbf{a}_1}_{\text{Regular } 50\Omega \text{ nonlinear distortion}} + \underbrace{\mathbf{S}_{22}(|\mathbf{a}_1|)\mathbf{S}_{ant}\mathbf{b}_2 + \mathbf{T}_{22}(\mathbf{a}_1)\mathbf{S}_{ant}^*\mathbf{b}_2^*}_{\text{Antenna coupling and mismatch effects}}$$

## Far field radiation

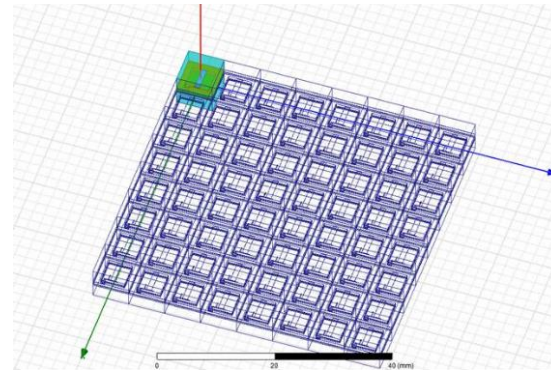
$$E_{tot}(El, Az)[n] = \sum_{i=1}^N b_{2,i}[n] \bar{E}_i(El, Az)$$

# Phased array example

IC design



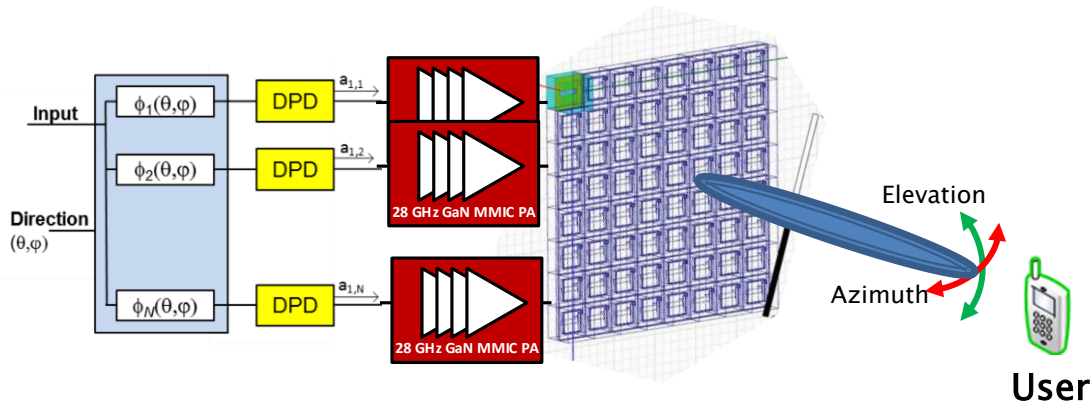
64 element antenna array



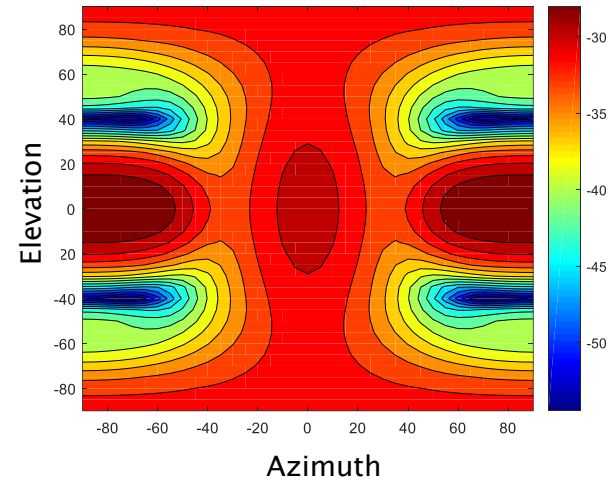
- PA model extracted from IC CAD
- Antenna parameters from EM CAD
- Each PA perfectly linearized for 50Ω load ( $a_2 = 0$ )
- Ideal phased array beam steering. No amplitude tapering

[C. Fager et al., "Analysis of Nonlinear Distortion in Phased Array Transmitters," Proc. INMMiC, 2017]

# Phased array example

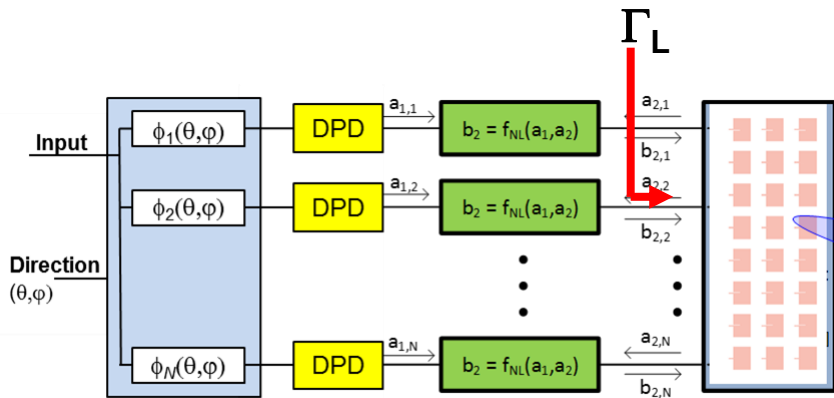


User EVM vs. scan direction

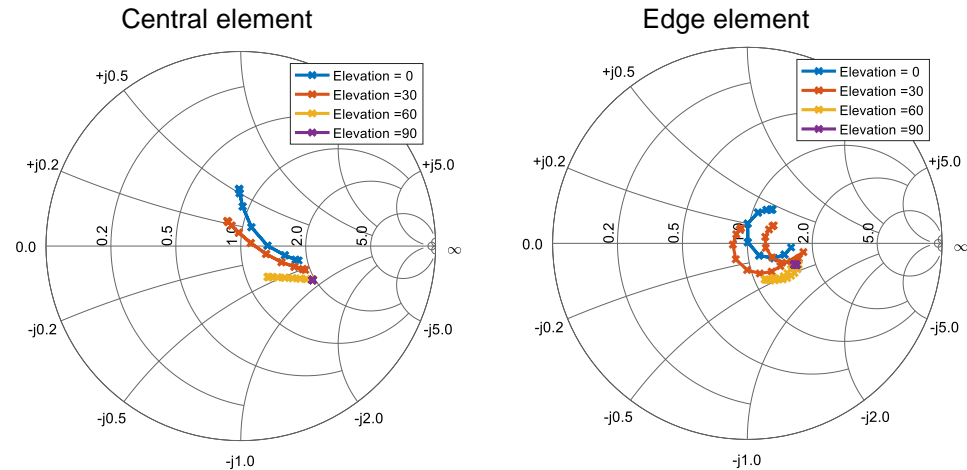


- Distortion highly direction dependent. *Why?*

# Phased array example



## $\Gamma_L$ vs. scan direction

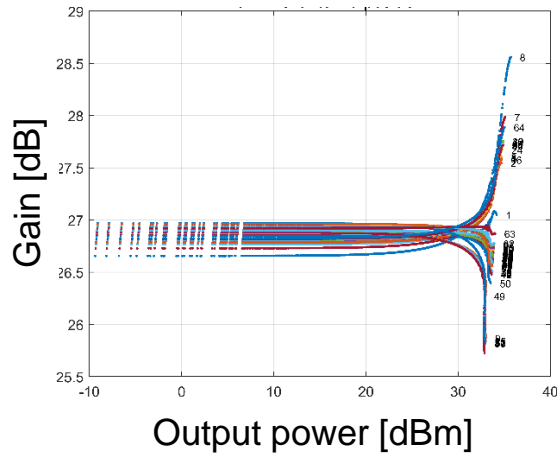


- Significant variation of PA load impedance vs. beam steering

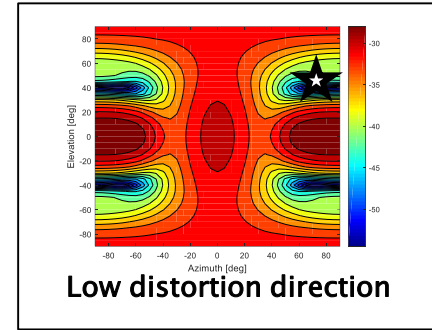
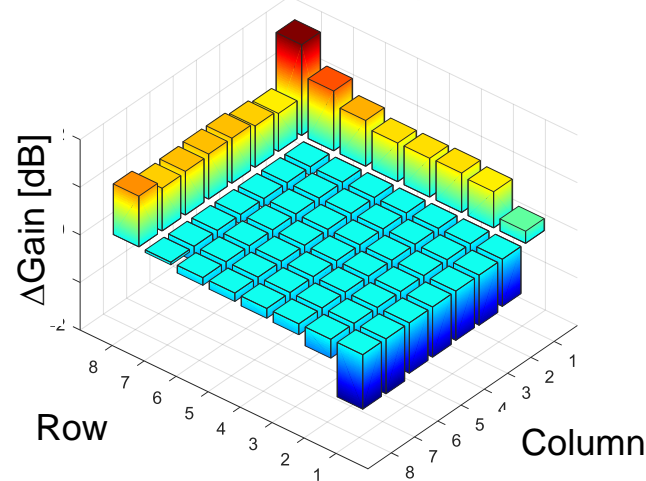


# Phased array example

AM/AM for each of the 64 branches



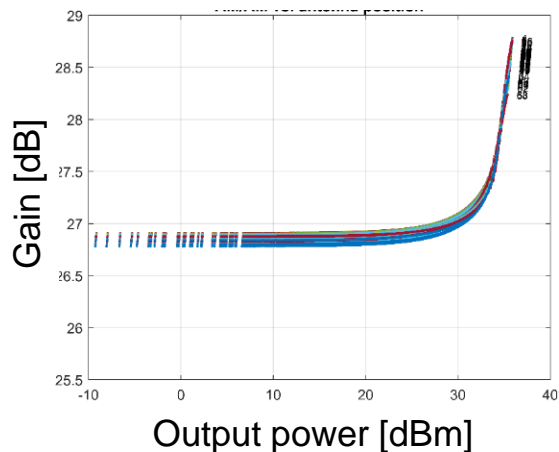
Gain compression/expansion



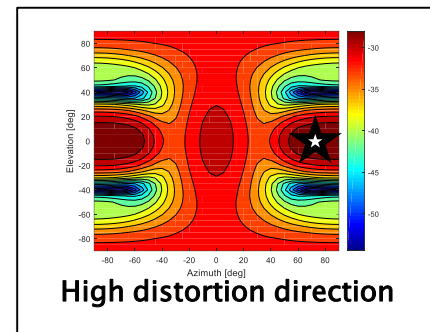
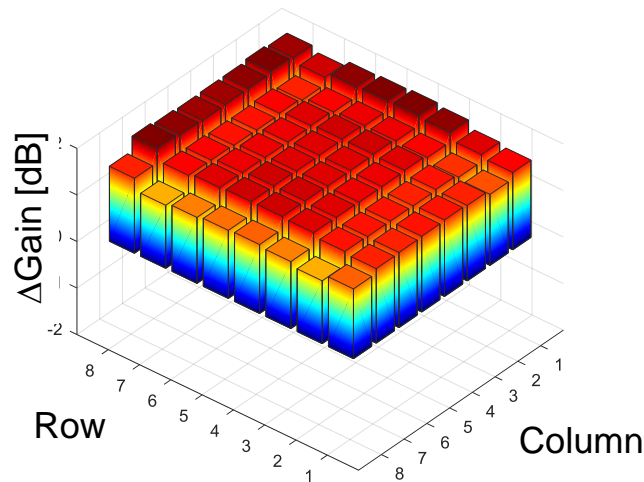
- Distortion averaging effects happening inside the array

# Phased array example

AM/AM for each of the 64 branches

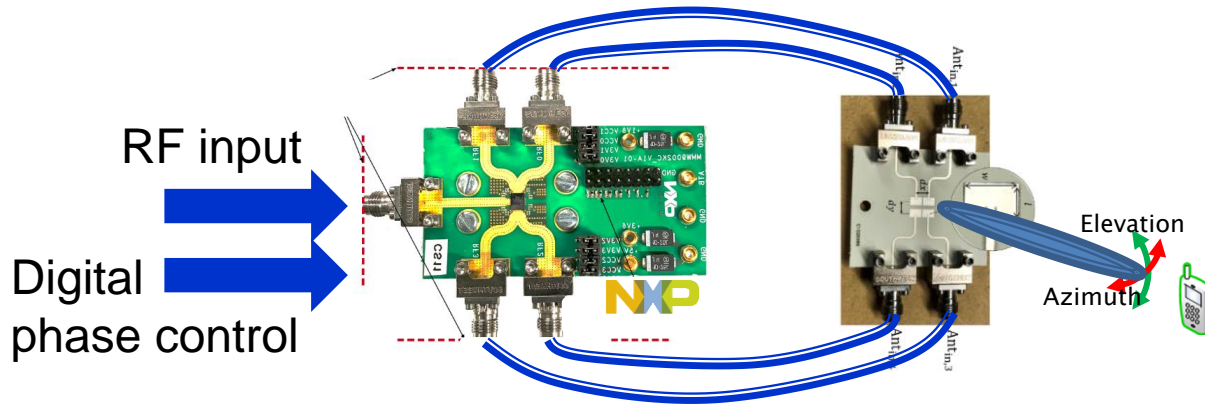


Gain compression/expansion

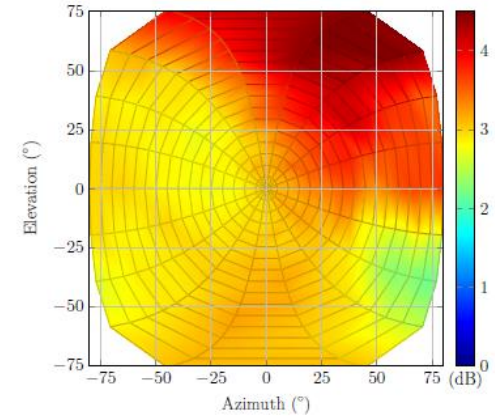


- Distortion addition for some directions
- Direction dependent user distortion → Direction dependent DPD needed

# Experimental verification

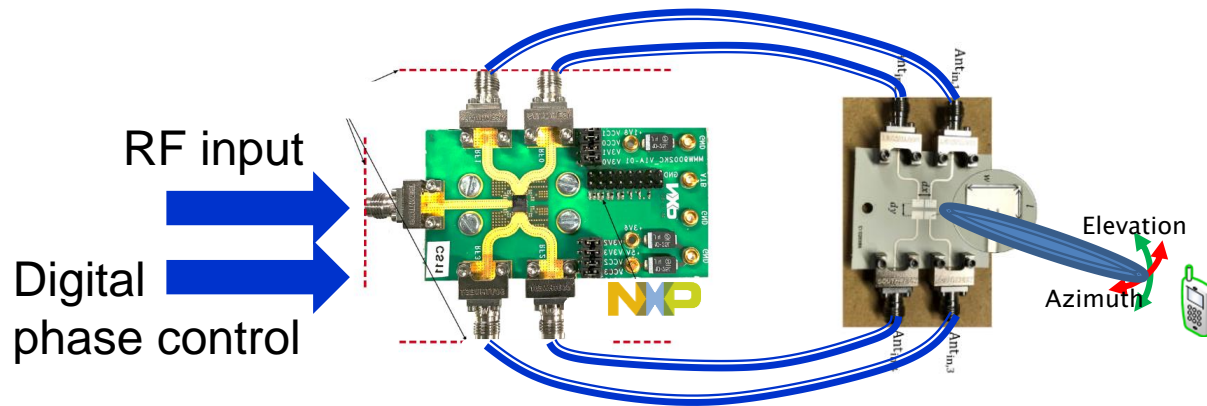


## AM-AM compression measurement

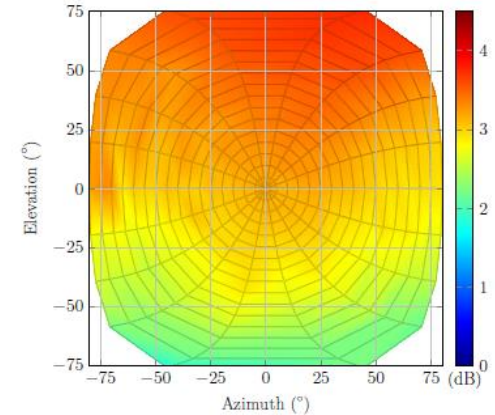


- Nonlinear effects observed also in mm-wave measurements
- 30 GHz beamforming chip

# Experimental verification

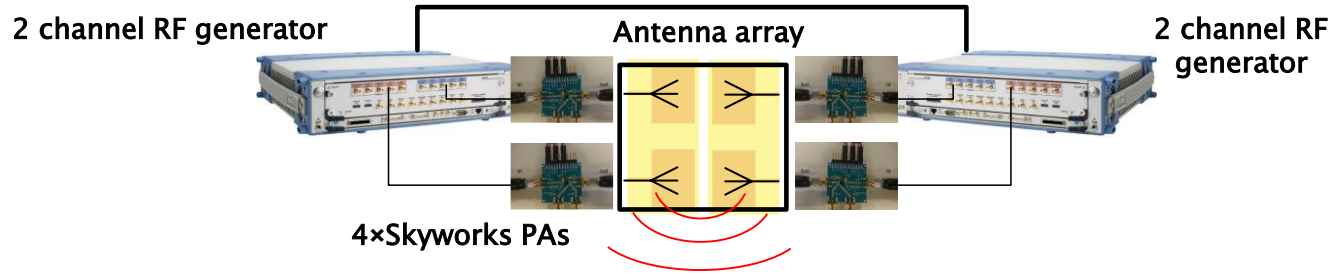


## AM-AM compression modeling

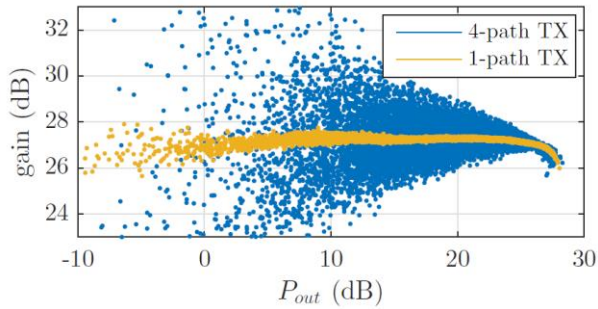


- Load-pull based nonlinear modeling
- 4 element patch antenna: EM simulation based modeling
- Reasonable modeling accuracy

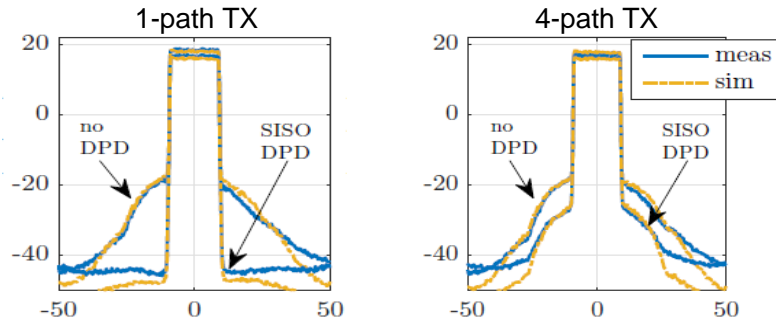
# MIMO transmitter distortion



## Nonlinear PA-antenna interactions

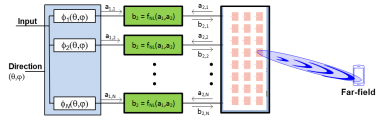


## Far field distortion

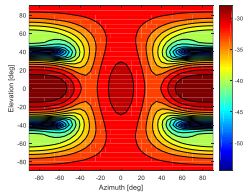
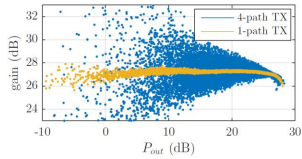


[K. Hausmair et al. "Prediction of Nonlinear Distortion in Wideband Active Antenna Arrays," IEEE T-MTT, 2017]

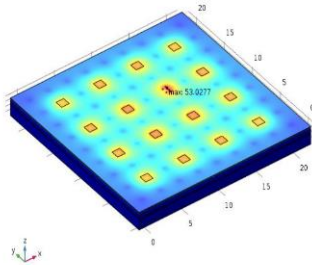
# Summary – transmitter RF modeling



- Framework for efficient simulation of active antenna systems
- Improved understanding of circuits-antenna interactions with realistic signals
- New nonlinear effects predicted in phased array and MIMO systems



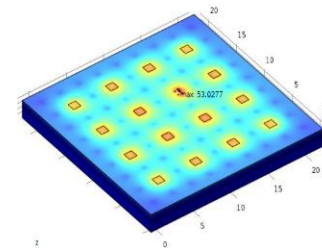
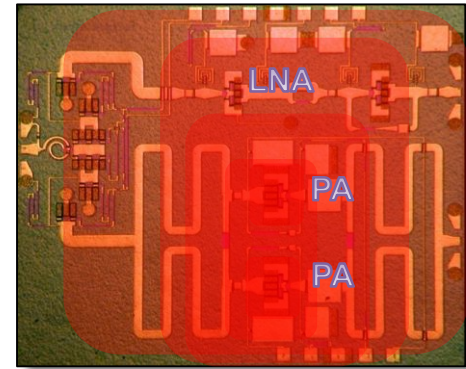
# ELECTRO-THERMAL SIMULATIONS



Thermal modeling  
Power dissipation modeling  
mm-wave transmitter example

# Heating concerns

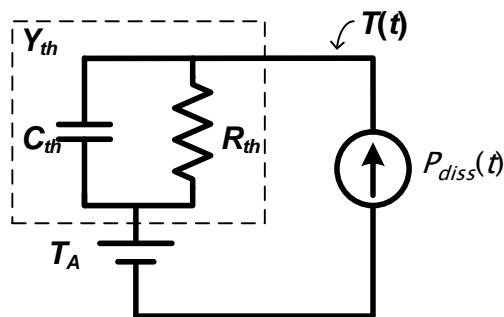
- Heat concentration in active antenna arrays
- Chip level heating effects
  - ◆ Thermal coupling
  - ◆ Efficient power amplifiers
- System level effects
  - ◆ Performance degradation
  - ◆ Reliability



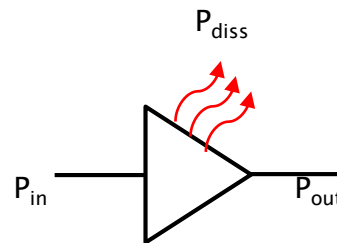


# Linear heating model

Thermal model



RF Model

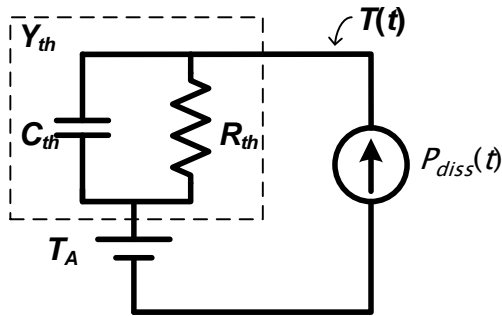


$$P_{diss}(t) = P_{diss}(|a_1(t)|, T(t))$$

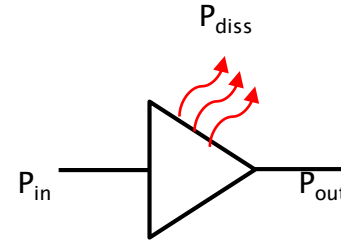
- $T(t) = T_A + P_{diss}(t) * z_{th}$
- Thermal admittance:  $Y_{th} = G_{th} + j\omega C_{th}$

# Linear heating model

Thermal model



RF Model

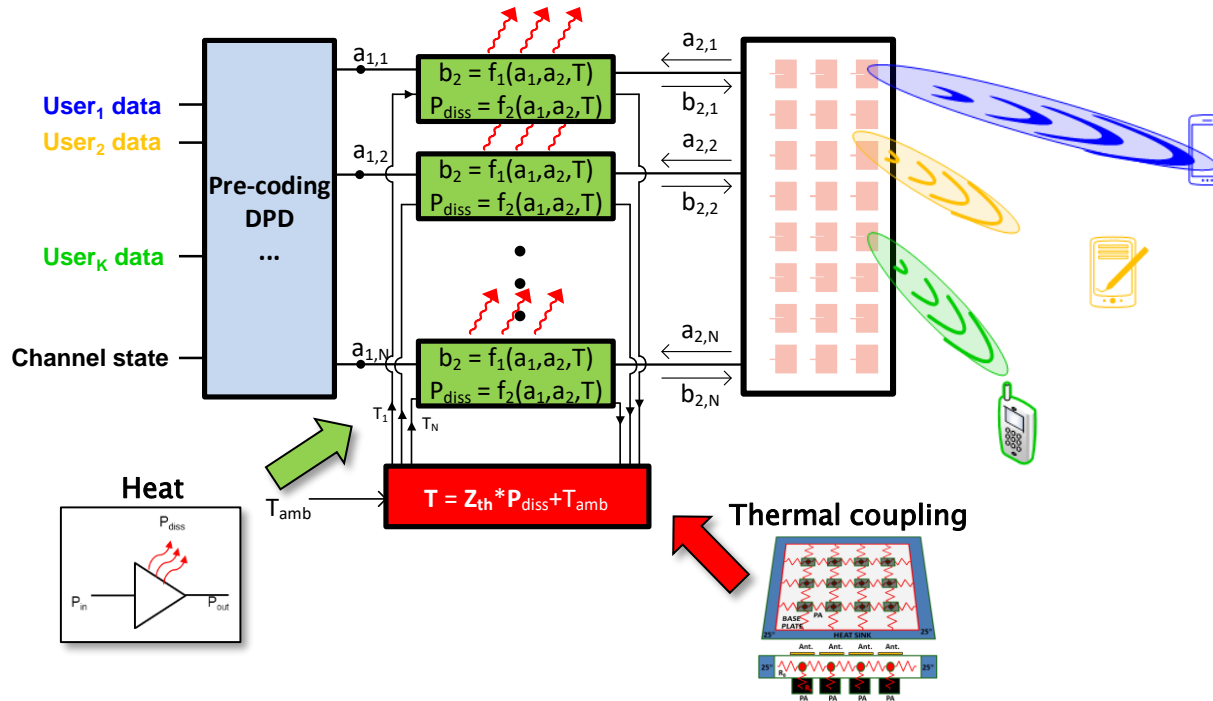


$$P_{diss}(t) = P_{diss}(|a_1(t)|, T(t))$$

- Envelope time-stepped solution for  $T(t)$

$$\mathbf{T}_{n+1} = T_{amb} + \left( \mathbf{G}_{th} + 2\pi f_s \mathbf{C}_{th} \right)^{-1} \left( \mathbf{P}_{diss,n} + 2\pi f_s \mathbf{C}_{th} \left( \mathbf{T}_n - T_{amb} \right) \right)$$

# Incorporating thermal effects



[C. Fager et al. "Analysis of Thermal Effects in Active Antenna Array Transmitters...", *Proc. INMMiC*, 2015]

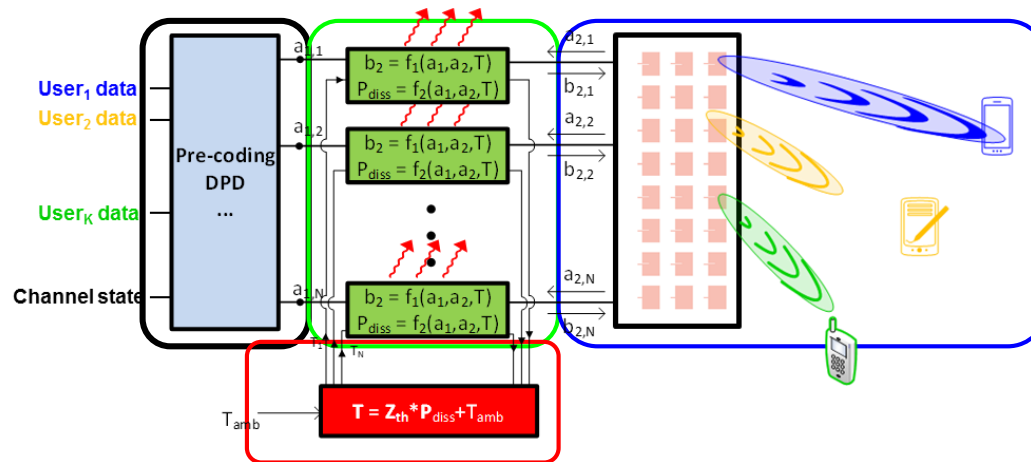
# Combined RF/EM/Thermal simulation

$$\mathbf{a}_{1,n} = \mathbf{G}\mathbf{x}_n$$

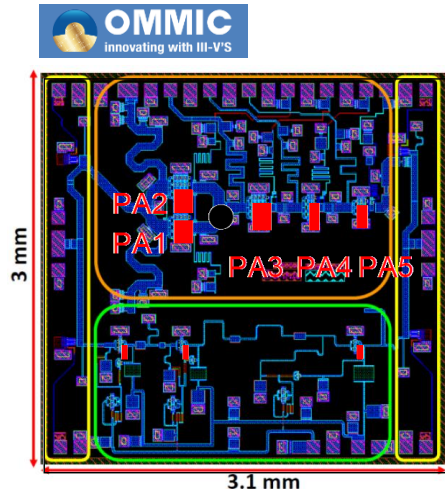
$$\mathbf{b}_{2,n} = \mathbf{S}_{21}(|\mathbf{a}_{1,n}|, \mathbf{T}_n)\mathbf{a}_{1,n} + \mathbf{S}_{22}(|\mathbf{a}_{1,n}|, \mathbf{T}_n)\mathbf{S}_{ant}\mathbf{b}_{2,n} + \mathbf{T}_{22}(\mathbf{a}_{1,n}, \mathbf{T}_n)\mathbf{S}_{ant}^*\mathbf{b}_{2,n}^* + \boldsymbol{\rho}_{n-1}$$

$$E_n(\theta, \varphi) = \mathbf{b}_{2,n}^T \bar{\mathbf{E}}(\theta, \varphi)$$

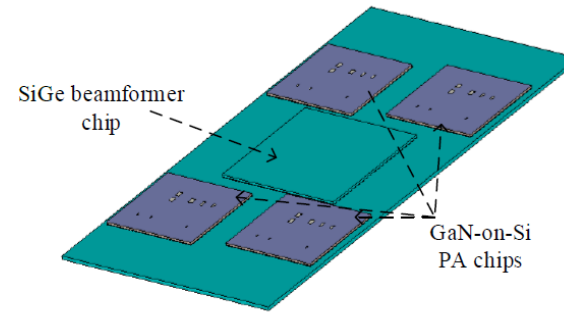
$$\mathbf{T}_{n+1} = T_{amb} + (\mathbf{G}_{th} + 2\pi f_s \mathbf{C}_{th})^{-1} (\mathbf{P}_{diss,n}(|\mathbf{a}_{1,n}|, \mathbf{T}_n) + 2\pi f_s \mathbf{C}_{th} (\mathbf{T}_n - T_{amb}))$$



# Example: SERENA 4-channel transmitter

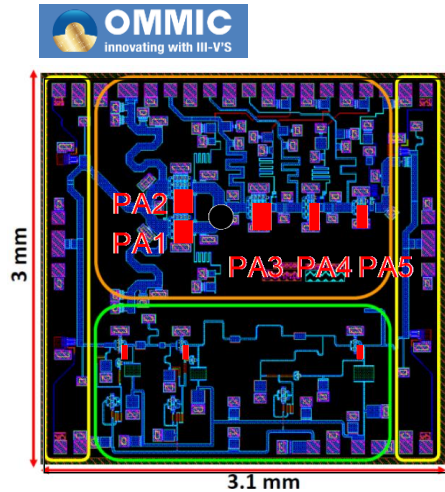


1. PA1:  $8 \times 115 \mu\text{m} = 920 \mu\text{m} (\approx 0.255w_{\text{tot}})$
2. PA2:  $8 \times 115 \mu\text{m} = 920 \mu\text{m} (\approx 0.255w_{\text{tot}})$
3. PA3:  $8 \times 115 \mu\text{m} = 920 \mu\text{m} (\approx 0.255w_{\text{tot}})$
4. PA4:  $8 \times 57 \mu\text{m} = 456 \mu\text{m} (\approx 0.126w_{\text{tot}})$
5. PA5:  $6 \times 65 \mu\text{m} = 390 \mu\text{m} (\approx 0.108w_{\text{tot}})$



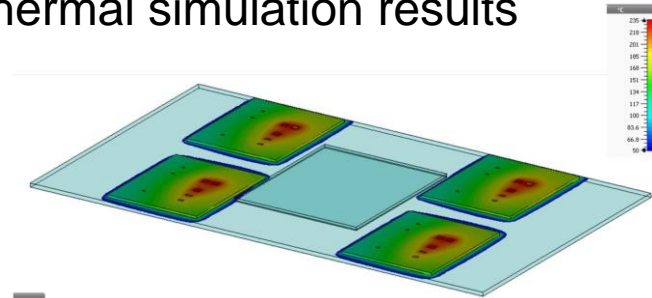
Material	Density $\rho$ (kg/m <sup>3</sup> )	Thermal conductivity $k$ (W/m·K)	Specific heat $C_p$ (J/kg·K)
Megtron 7	1820	0.4	0.88
Si	2330	148	0.7
SiGe	3950	8.8	0.5

# Example: SERENA 4-channel transmitter



1. PA1:  $8 \times 115 \mu\text{m} = 920 \mu\text{m}$  ( $\approx 0.255w_{\text{tot}}$ )
2. PA2:  $8 \times 115 \mu\text{m} = 920 \mu\text{m}$  ( $\approx 0.255w_{\text{tot}}$ )
3. PA3:  $8 \times 115 \mu\text{m} = 920 \mu\text{m}$  ( $\approx 0.255w_{\text{tot}}$ )
4. PA4:  $8 \times 57 \mu\text{m} = 456 \mu\text{m}$  ( $\approx 0.126w_{\text{tot}}$ )
5. PA5:  $6 \times 65 \mu\text{m} = 390 \mu\text{m}$  ( $\approx 0.108w_{\text{tot}}$ )

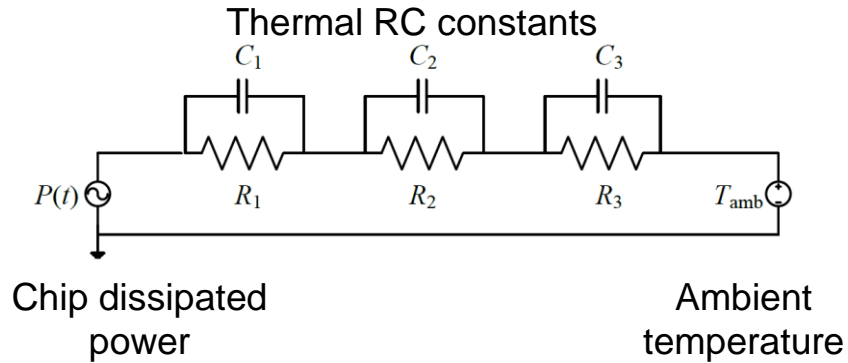
## Thermal simulation results



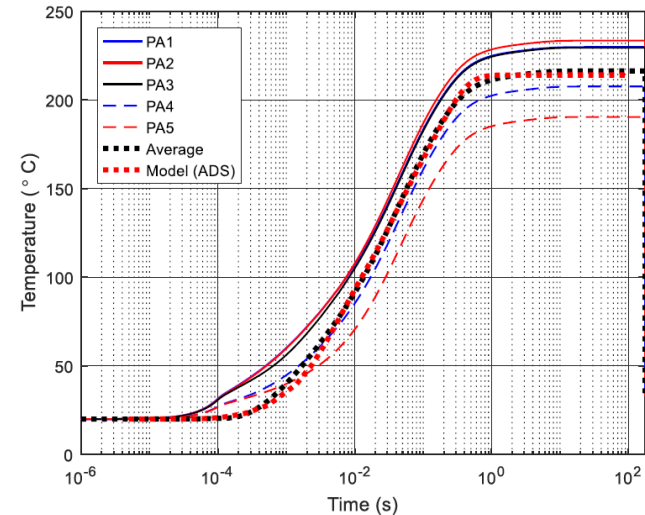
Material	Density $\rho$ (kg/m <sup>3</sup> )	Thermal conductivity $k$ (W/m·K)	Specific heat $C_p$ (J/kg·K)
Megtron 7	1820	0.4	0.88
Si	2330	148	0.7
SiGe	3950	8.8	0.5

# Thermal RC modeling

- One GaN chip in a simplified package environment

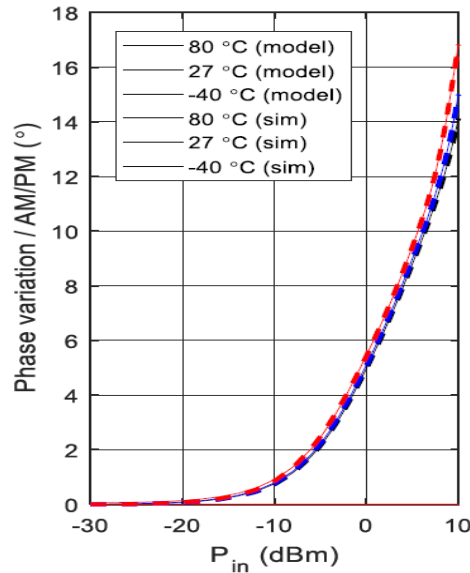
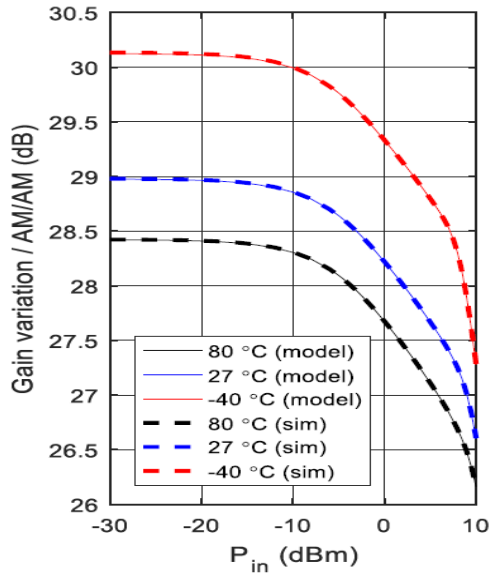


Thermal response @ 7W step



# Power amplifier modeling

- Temperature dependent gain

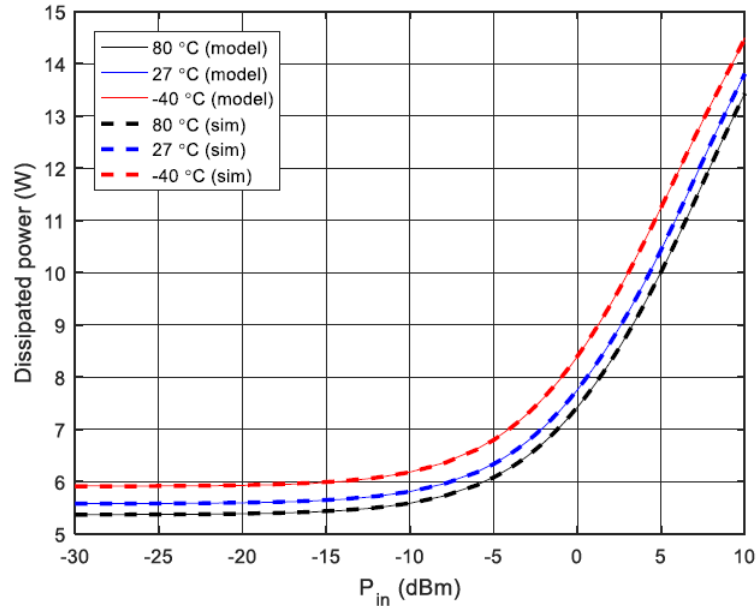


$$b_2(a_1, T) = \sum_{p_1=1}^{P_1} \alpha_{p_1}(T) a_1 |a_1|^{2(p_1-1)}$$



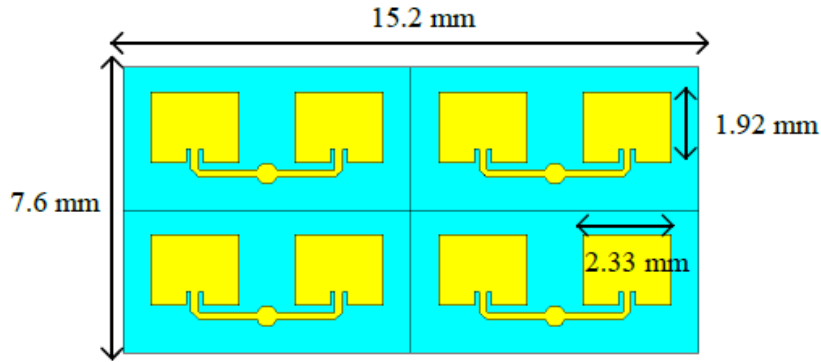
# Power amplifier modeling

- Dissipated power vs. temperature



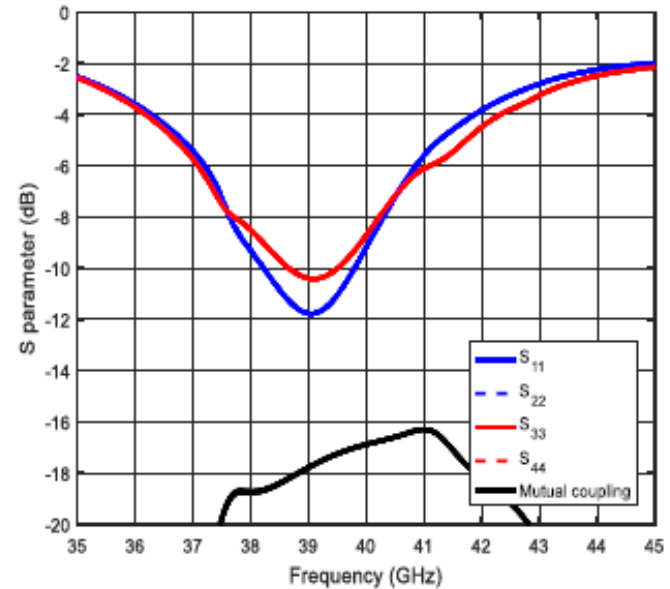
$$\begin{aligned}
 P_{\text{diss}}(|a_1|, T) &= P_{\text{dc}} + P_{\text{in}} - P_{\text{out}} \\
 &= \sum_{p_d=0}^{P_d} \xi_{p_d}(T) |a_1|^{p_d}
 \end{aligned}$$

# Antenna modeling

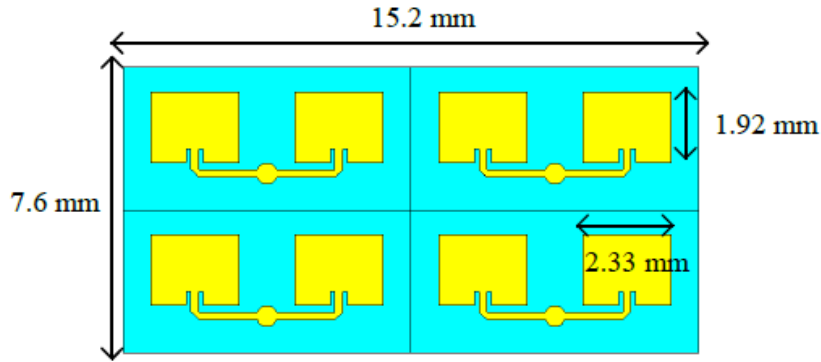


- Mismatch and mutual-coupling neglected in model

Simulated S-parameters

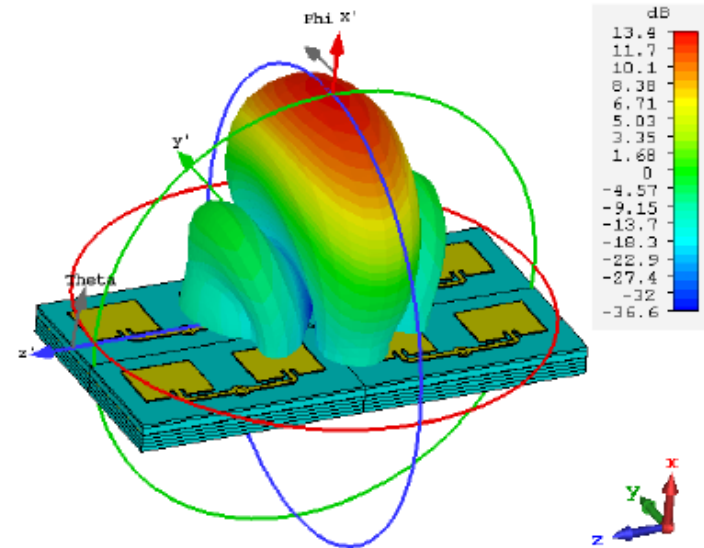


# Antenna modeling

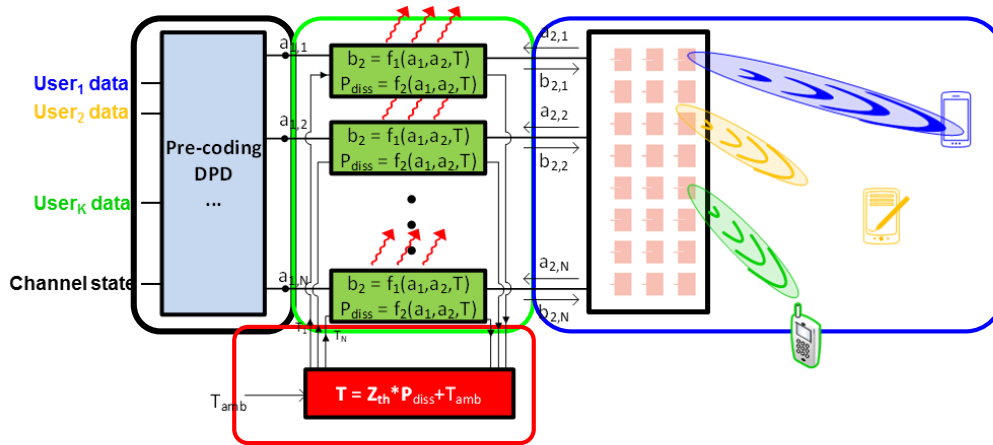


- Embedded element patterns for unity excitations

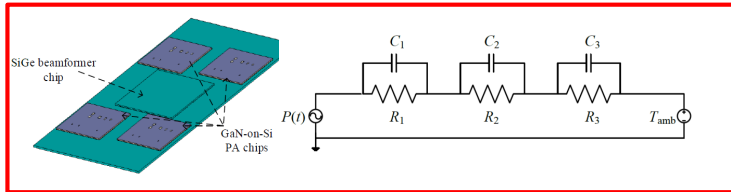
## Far-field radiation patterns



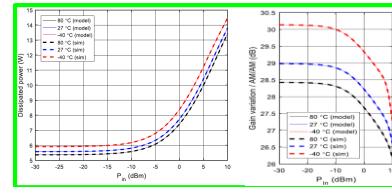
# Electro-thermal simulation framework



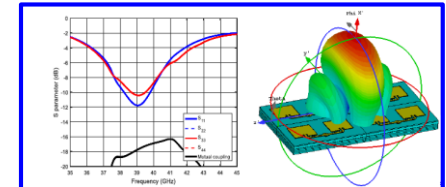
## Thermal modeling



## RF circuit modeling

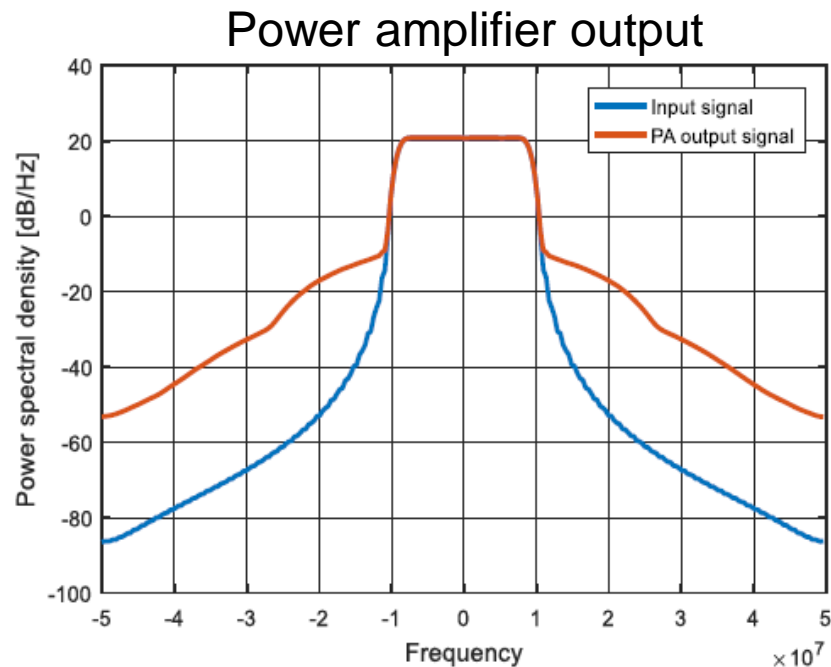


## Antenna modeling



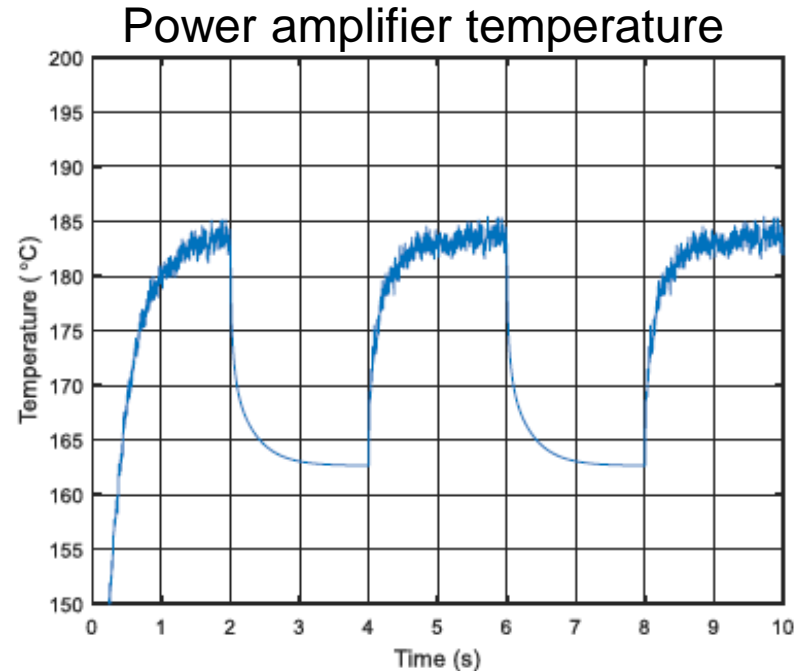
# Prediction of transmitter RF nonlinearities

- PA input-/output spectrum for modulated signals
- PA-to-PA nonlinear interactions

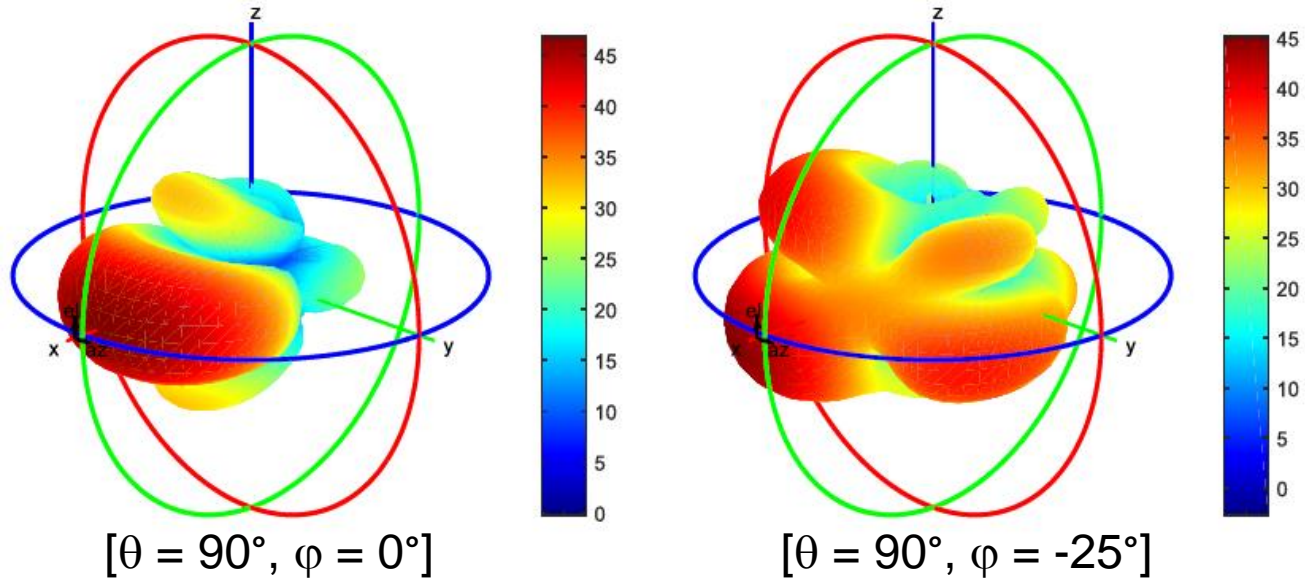


# Prediction of PA temperature dynamics

- Thermal transients
- On-off switching, e.g. between T/R in TDD systems
- Heat spreading in arrays

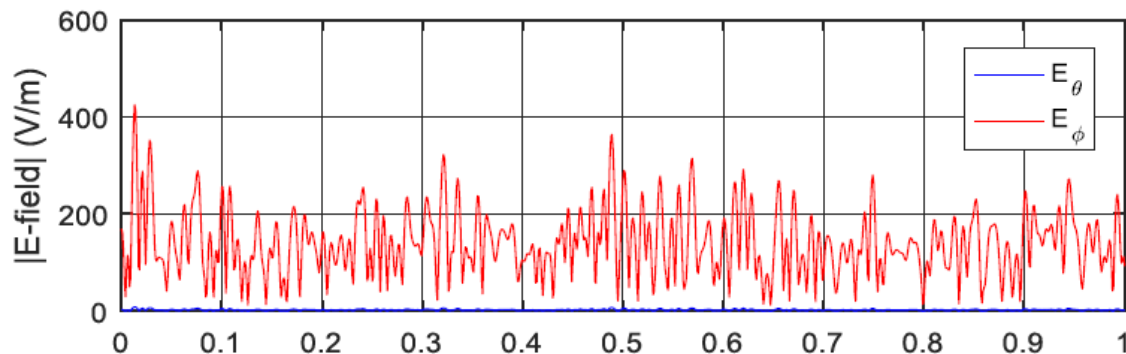


# Prediction of radiation patterns



# Prediction of modulated field at user

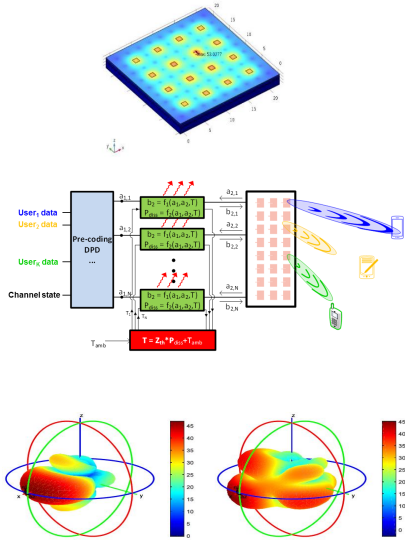
- Modulated fields in both polarizations considering both PA, thermal, antenna and beam-forming settings





# Summary – Electro-thermal simulations

- Thermal effects at circuit- and package levels
- Framework for electro-thermal transmitter simulations
- Prediction of joint electrical- and thermal effects in mm-wave antenna arrays



# CONCLUSIONS

# Conclusions

- mm-wave transmitter design is cross-disciplinary
  - ◆ Co-design between signals, circuits & antennas
- New nonlinear distortion phenomena
  - ◆ Both circuit and array level linearization needed
  - ◆ Low complexity MIMO linearization proposed
- Power dissipation a great challenge
  - ◆ Thermal coupling effects
- Understanding linearity and power dissipation effects through accurate multi-physics simulations is critical for successful 5G system design

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## Acknowledgments



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